
DEVELOPMENT OF NON-PROPRIETARY ULTRA HIGH PERFORMANCE CONCRETE

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Sponsored by the Montana Department of Transportation

Introduction

Objectives

- Develop and characterize non-proprietary UHPC mixes with materials readily available in Montana
- Mix designs anticipated to be significantly less expensive than commercially available options
- MDT interested in using UHPC as field-cast jointing material for precast components – reduced bond length and subsequent joint spacing



<https://www.fhwa.dot.gov/publications/research/infrastructure/structures/11022/>

Introduction

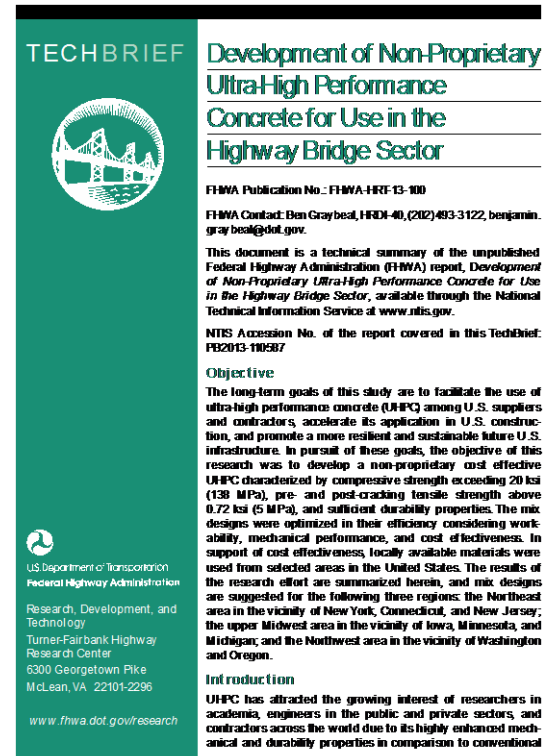
Scope

- Task 1 – Literature Review
- Task 2 – Response Surface Methodology to develop suitable UHPC mixes
- Task 3 – Characterize long-term mechanical and durability performance of selected UHPC mixes
- Task 4 - Reporting

Literature Review

Literature Review

- Extensive Research Documenting the Enhanced Performance of UHPC
 - Mechanical Properties
 - Durability
 - Structural Performance
- Non-Proprietary UHPC Research
 - Large-scale investigation completed by FHWA in 2013
 - Several state DOTs looking into this as well
 - Michigan
 - Nebraska
- Field Cast Joints
 - FHWA
 - Michigan



Materials

Materials

Portland Cement

- Type I/II Portland cement was used as the cementitious material
 - Sourced from the CRH Trident Plant



<https://www.thermofisher.com/blog/wp-content/uploads/2014/07/156638544.jpg>

Materials

Fly Ash

- Fly ash chosen as secondary supplemental cementitious material
 - Low cost relative to other supplemental materials
 - Can react pozzolonomically with hydration byproducts
 - Spherical shape helps with workability
 - Class F fly ash from Coal Creek Station



<http://www.brighthubengineering.com/concrete-technology/42969-what-is-fly-ash-concrete/>

Materials

Silica Fume

- MasterLife SF 100 from BASF was utilized for this experiment
 - BASF materials are readily available throughout Montana



[http://www.di-corp.com/public/uploads/product_files/Silica_Densified_\(3\)/1433380417-1280w_Silica_Densified_\(3\).JPG](http://www.di-corp.com/public/uploads/product_files/Silica_Densified_(3)/1433380417-1280w_Silica_Densified_(3).JPG)

Materials

Aggregates

- High quality aggregates required for UHPC
 - Masonry Sand from Quikcrete Plant in Billings
 - Good Gradation
 - Readily Available



Materials

High Range Water Reducer

- Fluid Premia 150 from CHYRSO, Inc. was chosen based on flow performance and reduction of entrapped air

CHRYSO®Fluid Premia 150

High range water reducing Super plasticizing admixture



CHRYSO®Fluid Premia 150 is a new generation superplasticizer based on modified polycarboxylate.

CHRYSO®Fluid Premia 150 has evolved from CHRYSO®Fluid Premia 100 and gives more water reduction for the same dosage.

CHRYSO®Fluid Premia 150 has been designed for use in precast concretes. When used in concretes which contain many fine particles, exceptional fluidity can be obtained, which greatly helps the laying of concrete, even without using vibrating techniques.

CHRYSO®Fluid Premia 150 produces concrete with very high early and long term strengths. When used in a specially formulated concrete, CHRYSO®Fluid Premia 150 can give hard concrete a first class finish.

Indicative characteristics

- Nature: liquid
- Colour: White
- Freezing point: 0 °C
- Ash content: ≤ 0,5%
- Shelf life: 9 months

Specifications

- Specific gravity (20°C): 1,060 ± 0,010
- pH: 5,00 ± 1,00
- Solid content (halogen): 29,00% ± 1,40%
- Solid content (EN 480-8): 29,00% ± 1,40%
- Na₂O equivalent: ≤ 1,00%
- Cl⁻ ions content: ≤ 0,10%

Norms and regulations

- This product conforms to CE marking. The appropriate declaration can be found on our internet site.

- This product conforms to NF 085 certification, which technical specifications are those applied in the non harmonised part of NF EN 934-2.
- This product doesn't have any effect on the corrosion of steel in concrete (electrochemical test according to DIN V 18998:2002-11).

Domains of application

- All cement types
- Self consolidating concrete
- High early strength
- High Performance Concrete
- Prestressed concrete
- Precast

Precautions

Protect from frost.
Avoid prolonged exposure to high temperatures.
Store in plastic containers, PVC excluded.
Should the product freeze, it will recover its properties. After thawing, an efficient agitation is necessary until the product is entirely homogeneous again.

Method of use

Dosage: 0.25 to 2.00 kg for 100 kg of cement.

This product must be added to the mixing water or at the end of the mixing cycle.

Should the product be added to fresh concrete, into the mixing truck, it is necessary to mix at high speed, for 1 minute per m³ of concrete (with a total minimum of 6 minutes).

Construction sites references

Car park in Terminal 2E, Roissy Charles de Gaulle Airport, France: prestressed SCC caissons.



Materials

Steel Fibers

- Nycon-SF Type I “Needles”
- 0.2 mm diameter by 13mm in length



Materials

Estimated Costs (rough estimate)

| Material | Manufacturer | Cost (per ton) |
|----------------------------|--------------|----------------|
| Fine Aggregate | QUIKRETE | \$26 |
| Portland Cement, Type I/II | CRH | \$145 |
| Silica Fume | BASF | \$840 |
| Fly Ash, Type F | Coal Creek | \$135 |
| HRWR (per gallon) | CHRYSO, Inc. | \$14 |
| Steel Fibers | Nycon | \$1,600 |

Methods

Methods

Mixing Procedure

- Modified mixing procedure required for UHPC
 - Aggregate and silica fume dry mixed for 5 minutes
 - Portland cement and fly ash added and mixed for an additional 5 minutes
 - Mix water and 1/3 HRWR added to mix
 - Remaining HRWR added within 1 minute
 - Mixing speed increased after turnover
 - Mixed until desired fluidity achieved, 5-10 additional minutes



Methods

Flow Testing

- Flow determined using ASTM C230 flow cone

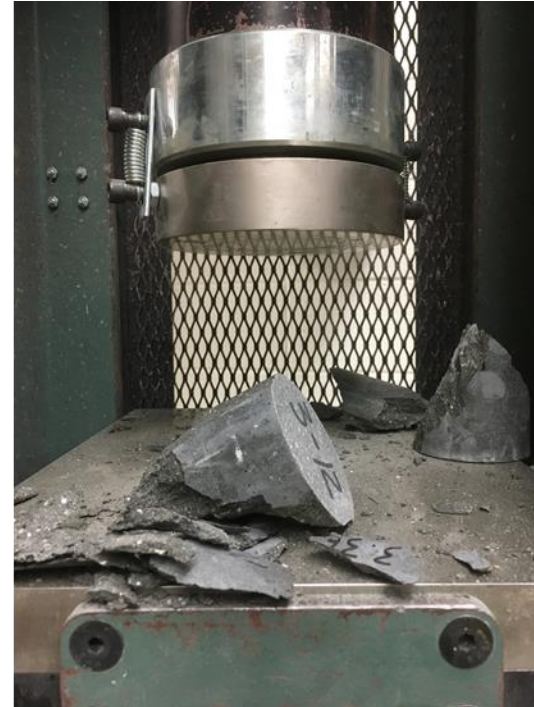


Methods

Specimen Preparation



Methods

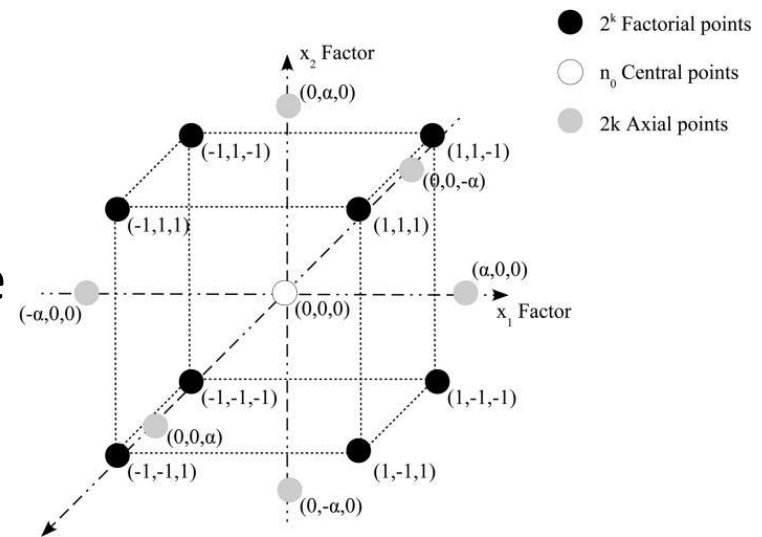


Experimental Design

Experimental Design

Response Surface Methodology

- Maximizes output while minimizing input
- RSM is used when the relationship between input variables and responses are not exactly known
- Especially useful when no mechanistic models are available



<http://manufacturingscience.asmedigitalcollection.asme.org/article.aspx?articleid=1440072>

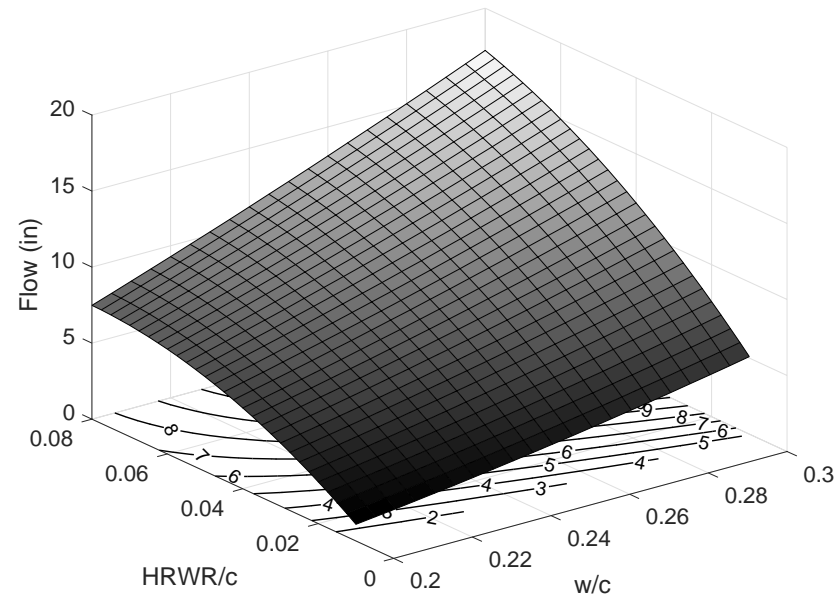
Experimental Design

| Mix ID | Independent Variables | | | | Measured Responses | | | |
|---------|-----------------------|--------------|-------------|--------------|--------------------|--------------------|----------------------|--------------------------------|
| | w/c Ratio | Sand/c Ratio | SF/FA Ratio | HRWR/c Ratio | Flow (inches) | 28-Day f_c (ksi) | Cost/yd ³ | Unit Wt. (lb/ft ³) |
| 27 C | 0.250 | 1.25 | 1.00 | 0.0450 | 8.50 | 18.05 | \$367.34 | 140.7 |
| 25 C | 0.250 | 1.25 | 1.00 | 0.0450 | 7.00 | 17.19 | \$367.34 | 142.7 |
| 12 | 0.275 | 1.50 | 1.15 | 0.0275 | 4.00 | 11.29 | \$314.88 | 139.9 |
| 14 | 0.275 | 1.00 | 1.15 | 0.0625 | 12.25 | 17.52 | \$429.97 | 138.5 |
| 16 | 0.275 | 1.50 | 1.15 | 0.0625 | 10.25 | 14.48 | \$379.60 | 140.5 |
| 4 | 0.225 | 1.50 | 1.15 | 0.0275 | 4.00 | 1.67 | \$326.42 | n/a |
| 23 | 0.250 | 1.25 | 0.70 | 0.0450 | 7.00 | 14.96 | \$346.64 | 141.5 |
| 17 | 0.200 | 1.25 | 1.00 | 0.0450 | 4.00 | 11.67 | \$382.05 | n/a |
| 6 | 0.225 | 1.00 | 1.15 | 0.0625 | 7.25 | 17.36 | \$448.16 | 140.9 |
| 15 | 0.275 | 1.50 | 0.85 | 0.0625 | 8.75 | 16.91 | \$363.44 | 143.0 |
| 1 | 0.225 | 1.00 | 0.85 | 0.0275 | 4.00 | 6.61 | \$351.01 | n/a |
| 26 C | 0.250 | 1.25 | 1.00 | 0.0450 | 7.50 | 17.03 | \$367.34 | 142.5 |
| 20 | 0.250 | 1.25 | 1.00 | 0.0800 | 9.50 | 16.28 | \$437.40 | 141.0 |
| 19 | 0.250 | 1.25 | 1.00 | 0.0100 | 4.00 | 0.41 | \$296.26 | n/a |
| 11 | 0.275 | 1.50 | 0.85 | 0.0275 | 4.00 | 3.36 | \$298.69 | n/a |
| 24 | 0.250 | 1.25 | 1.30 | 0.0450 | 7.75 | 17.03 | \$382.69 | 141.7 |
| 5 | 0.225 | 1.00 | 0.85 | 0.0625 | 11.00 | 17.57 | \$428.59 | 142.2 |
| 8 | 0.225 | 1.50 | 1.15 | 0.0625 | 5.00 | 16.82 | \$393.41 | 144.0 |
| 2 | 0.225 | 1.00 | 1.15 | 0.0275 | 4.00 | 5.57 | \$370.62 | 133.6 |
| 22 | 0.250 | 1.75 | 1.00 | 0.0450 | 5.25 | 14.26 | \$327.32 | 142.4 |
| 21 | 0.250 | 0.75 | 1.00 | 0.0450 | 12.50 | 18.89 | \$421.28 | 138.7 |
| 13 | 0.275 | 1.00 | 0.85 | 0.0625 | 11.50 | 17.40 | \$411.21 | 139.6 |
| 3 | 0.225 | 1.50 | 0.85 | 0.0275 | 4.00 | 2.66 | \$309.62 | n/a |
| 7 | 0.225 | 1.50 | 0.85 | 0.0625 | 9.25 | 18.49 | \$376.64 | 144.9 |
| 9 | 0.275 | 1.50 | 0.85 | 0.0275 | 4.00 | 8.37 | \$298.69 | 137.8 |
| 10 | 0.275 | 1.00 | 1.15 | 0.0275 | 5.75 | 16.32 | \$355.46 | 139.7 |
| 18 | 0.300 | 1.25 | 1.00 | 0.0450 | 13.00 | 18.16 | \$353.73 | 139.3 |
| Min. | 0.200 | 0.75 | 0.70 | 0.0100 | 4.00 | 0.41 | \$296.26 | 133.6 |
| Max. | 0.300 | 1.75 | 1.30 | 0.0800 | 13.00 | 18.89 | \$448.16 | 144.9 |
| Average | 0.250 | 1.27 | 1.00 | 0.0450 | 7.22 | 13.20 | \$366.88 | 140.7 |
| CV | - | - | - | - | 0.43 | 0.45 | 0.12 | 0.02 |

Experimental Design

Initial Experimental Design

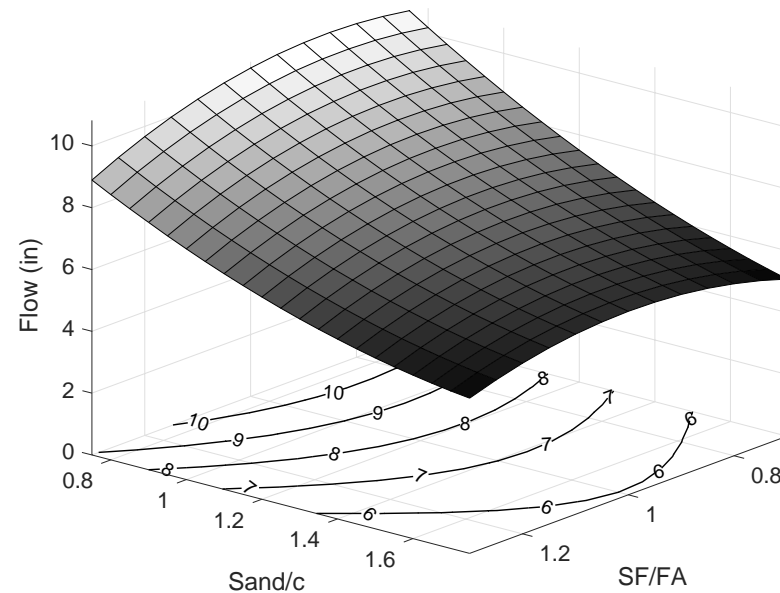
- Response Surfaces
 - Flow vs. HRWR/c and w/c



Experimental Design

Initial Experimental Design

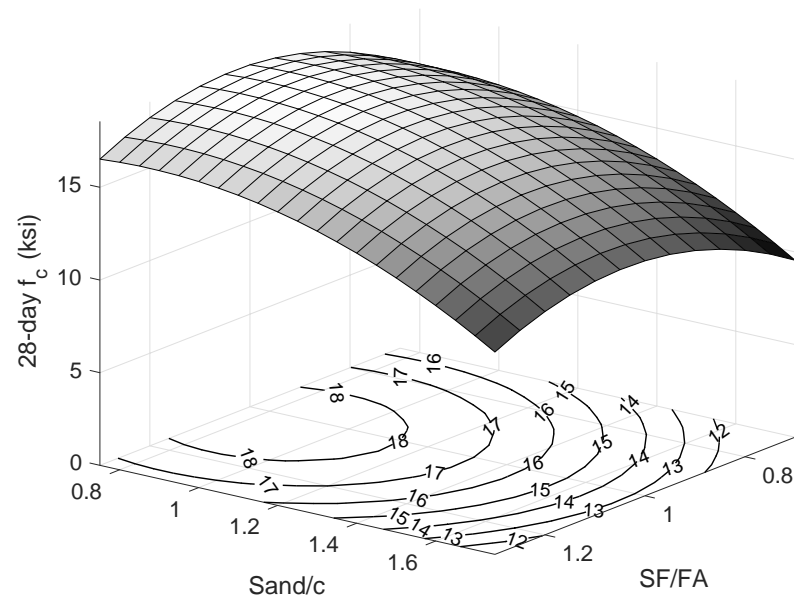
- Response Surfaces
 - Flow vs. sand/c and SF/FA



Experimental Design

Initial Experimental Design

- Response Surfaces
 - 28-day compressive strength vs. sand/c and SF/FA



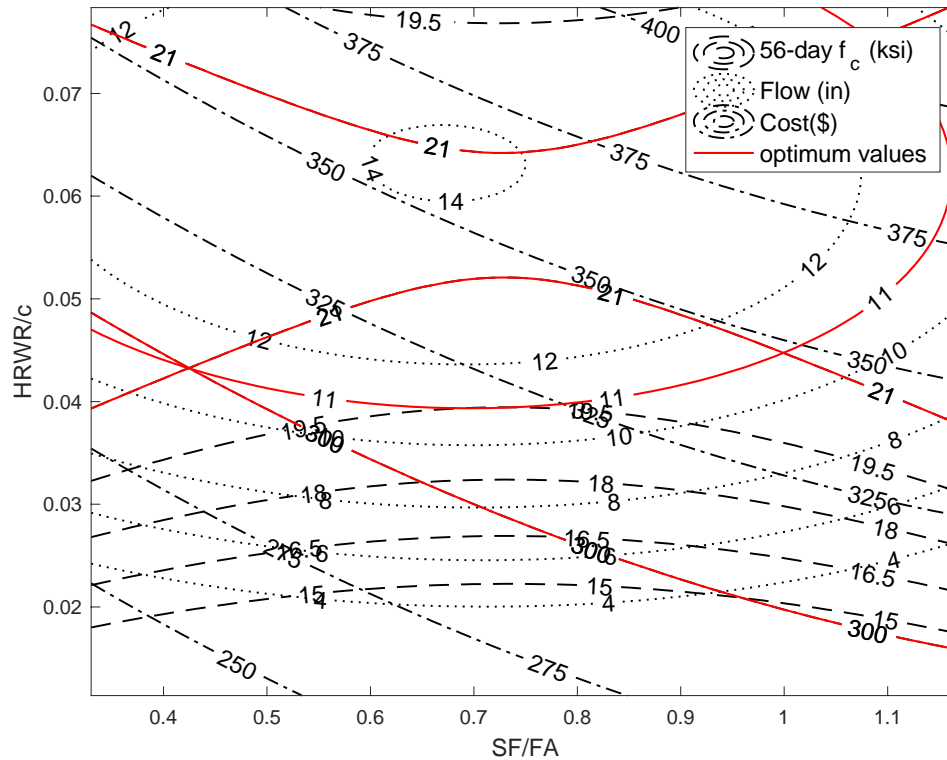
Mix Optimization

Mix Optimization

Mix Optimization

- Targeted Responses
 - Flow of 10 inches
 - Compressive Strength of 20 – 21 ksi
 - Cost of \$300-350
- Independent Variables
 - w/c ratio
 - HRWR/c ratio
 - SF/FA ratio

Mix Optimization



Mix Optimization

Mix Optimization

| Variable/Response | 3M1 | | 3M2 | | 3M3 | | 3M4 | |
|--------------------|------------------------|----------|------------------------|----------|------------------------|----------|------------------------|----------|
| w/c Ratio | 0.236 | | 0.237 | | 0.274 | | 0.216 | |
| SF/FA Ratio | 0.38 | | 0.31 | | 0.43 | | 0.68 | |
| HRWR/c Ratio | 0.042 | | 0.046 | | 0.043 | | 0.049 | |
| | Predicted (95% CI) | Measured | Predicted (95% CI) | Measured | Predicted (95% CI) | Measured | Predicted (95% CI) | Measured |
| Flow (inches) | 11.00 (8.9 to 13.1) | 12.00 | 11.00 (8.2 to 13.8) | 11.25 | 11.00 (7.0 to 15.0) | 12.50 | 11.0 (9.2 to 12.9) | 10.50 |
| 7-day f_c (ksi) | 14.4 (11.6 to 17.3) | 13.0 | 14.6 (10.9 to 18.3) | 14.1 | 16.3 (11.0 to 21.6) | 14.4 | 15.2 (12.7 to 17.6) | 11.2 |
| 28-day f_c (ksi) | 18.7 (15.5 to 22.0) | 16.2 | 19.4 (15.1 to 23.7) | 18.2 | 20.7 (14.6 to 26.9) | 18.2 | 19.1 (16.2 to 22.0) | 15.1 |
| 56-day f_c (ksi) | 20.0 (17.3 to 22.7) | 16.9 | 21.0 (17.5 to 24.5) | 18.2 | 21.0 (15.9 to 26.0) | 20.4 | 20.0 (17.6 to 22.3) | 18.6 |

Scaled-Up Trial Mixes, Mix Selection

- Scaled-up Mixes
 - All trial batches 0.2 cu. ft
 - Increased to 1.5 cu. ft
 - initially with fixed-fane rotation-drum concrete mixer
 - horizontal fixed-drum rotation-fin mortar mixer
 - Varied properties
 - flows and strengths off
 - Center-point performed best



Scaled-Up Trial Mixes, Mix Selection

- Variability between mixes and specimens
 - Specimen preparation
 - film forming on surface – moisture loss
 - continuously agitate and cover with plastic wrap
 - cut top end off hardened cylinder before grinding
 - entrapped air
 - Inclusion of steel fibers
 - increased ductility
 - reduced variability between specimens
 - Left in molds for 48 hours rather than 24



Mechanical and Durability Properties

Selected Mix

Mix Parameters

| w/c Ratio | Sand/c Ratio | SF/FA Ratio | HRWR/c Ratio |
|-----------|--------------|-------------|--------------|
| 0.240 | 1.40 | 0.75 | 0.045 |

Mix Proportions

| Mix Weights | | |
|---------------------|--------------------|------------------|
| Item | Fraction of Volume | Mix Weight (lbs) |
| Water | 0.16 | 2.011 |
| HRWR | 0.03 | 0.4332 |
| Retarder/Stabilizer | 0.00 | 0.0000 |
| Portland Cement | 0.24 | 9.63 |
| Silica Fume | 0.08 | 2.06 |
| Fly Ash | 0.11 | 2.75 |
| Fine Aggregate | 0.36 | 11.53 |
| Steel Fibers | 0.02 | 1.95 |

Rough Cost Estimate

| Cubic Yard Calculations | | | |
|-------------------------|---------------|------------|-------------|
| | Mix Wt. (lbs) | Cost/ton | Cost/Cu. Yd |
| Water | 271.5 | \$0.000000 | \$0.000000 |
| HRWR (gallons) | 6.74 | \$4.00 | \$4.37 |
| Portland Cement | 1299.5 | \$45.00 | \$4.21 |
| Silica Fume | 278.5 | \$40.00 | \$16.95 |
| Fly Ash | 371.3 | \$35.00 | \$5.06 |
| Fine Aggregate | 1556.4 | \$6.00 | \$20.23 |
| Steel Fibers | 262.8 | \$1,600.00 | \$10.26 |
| | | Total | \$61.09 |

Testing Protocol

Mechanical Properties

| Material Property | ASTM Test Method |
|----------------------------|------------------|
| Compressive Strength | C39 |
| Elastic Modulus | C469 |
| Modulus of Rupture | C78 |
| Splitting Tensile Strength | C496 |
| Shrinkage | C512 |

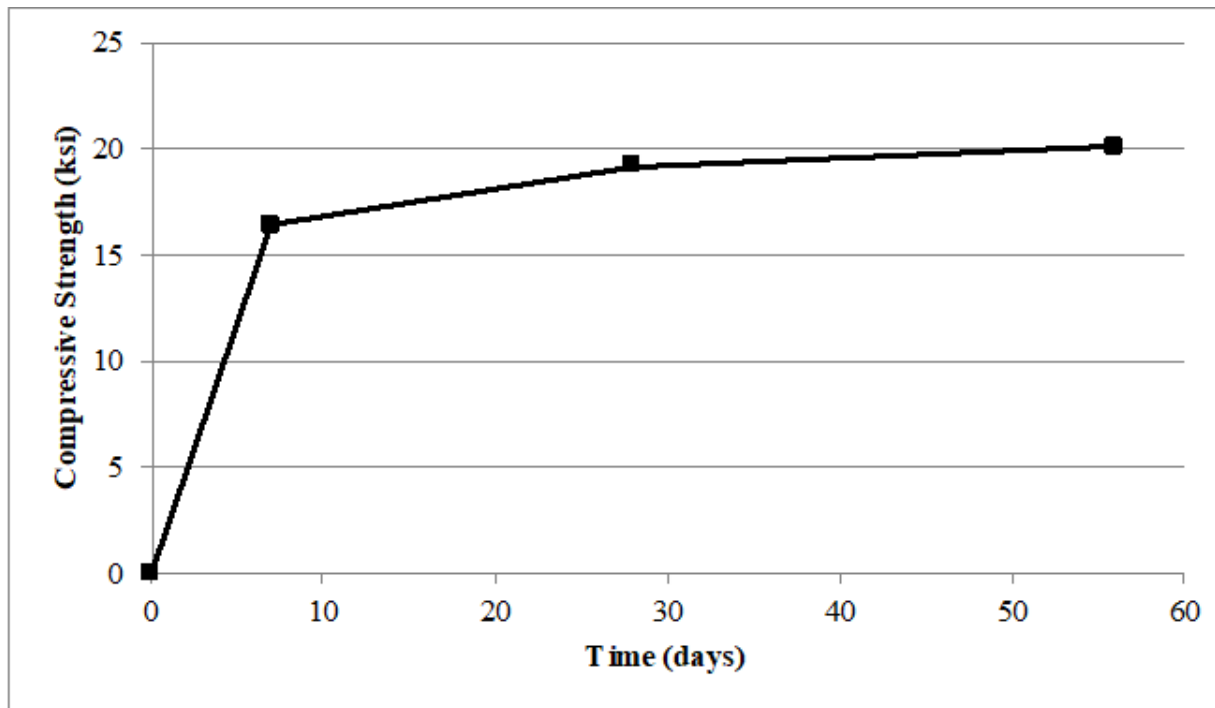


Durability Properties

| Durability Property | ASTM Test Method |
|--------------------------|------------------|
| Abrasion | C944 |
| Absorption | C642 |
| Alkali Silica Reactivity | C1567 |
| Chloride Penetration | C1202 |
| Freeze-Thaw | C666 |
| Scaling | C672 |

Unconfined Compressive Strength

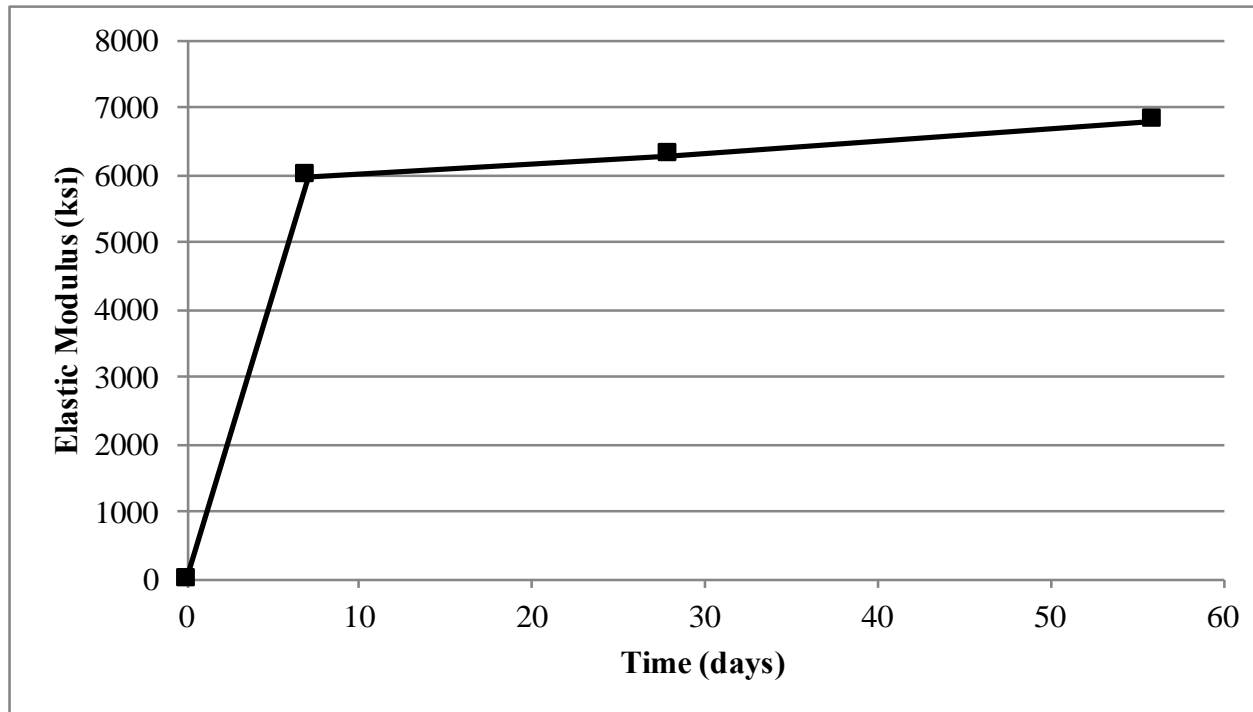
| Age (days) | f'_c (ksi) |
|------------|--------------|
| 7 | 16.4 |
| 28 | 19.2 |
| 56 | 20.1 |



Elastic Modulus

Predictive ACI Equation: $E_c = w_c^{1.5} 33 \sqrt{f'_c}$

| Age (days) | f'_c (ksi) | E_{Meas} (ksi) | E_{Pred} (ksi) | $\frac{E_{Meas}}{E_{Pred}}$ |
|------------|--------------|------------------|------------------|-----------------------------|
| 7 | 16.4 | 5977 | 7993 | 0.75 |
| 28 | 19.2 | 6289 | 8643 | 0.73 |
| 56 | 20.1 | 6787 | 8847 | 0.77 |



Flexural Tensile Strength

Predictive ACI Equation: $f_r = 7.5\sqrt{f'_c}$

28-day Results:

| Stress at Initial Crack (ksi) | Stress at Ultimate (ksi) | Predicted (ksi) | Meas/Predicted Initial | Meas/Predicted Ultimate |
|----------------------------------|-----------------------------|--------------------|---------------------------|----------------------------|
| 1.98 | 3.39 | 1.05 | 1.89 | 3.23 |

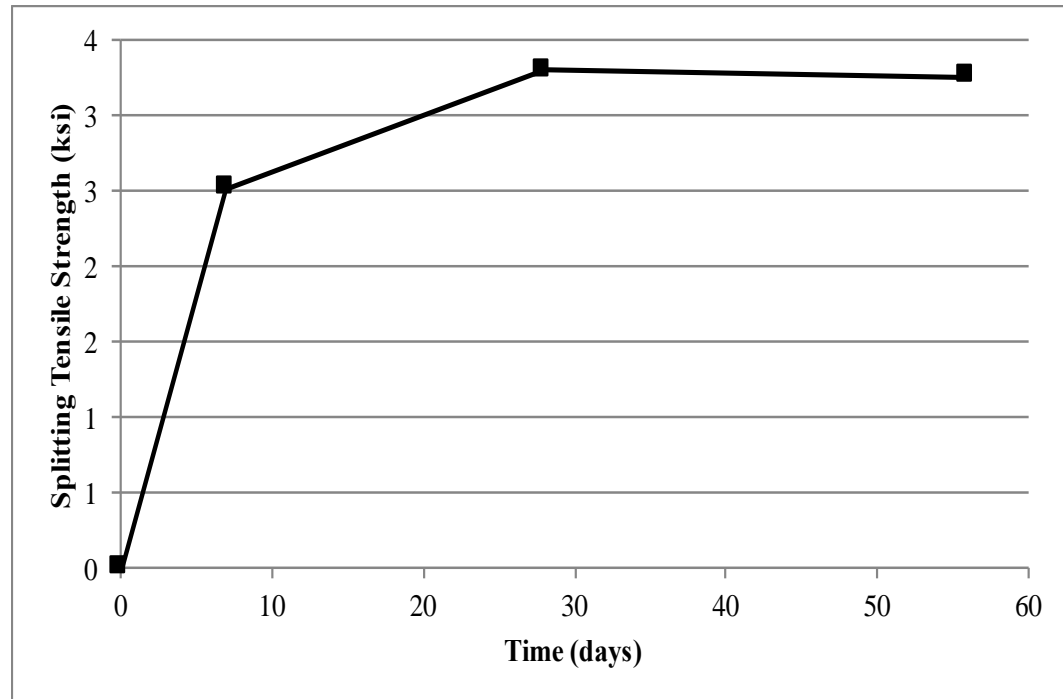


Splitting Tensile Strength

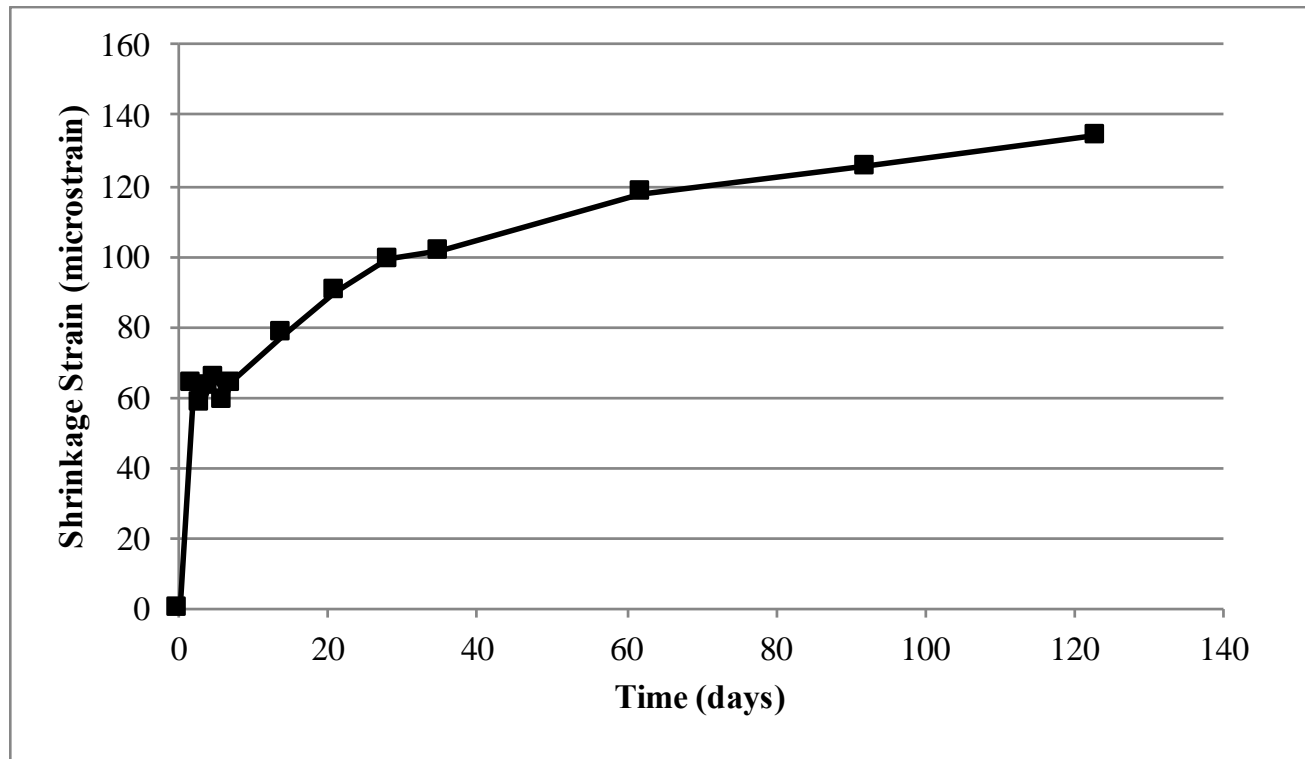
Predictive ACI Equation:

$$f_{ct} = 6.7\sqrt{f'_c}$$

| Age (days) | Stress at Ultimate (ksi) | Predicted at Initial Crack (ksi) | Meas/Predicted |
|------------|--------------------------|----------------------------------|----------------|
| 7 | 2.52 | 0.96 | 2.62 |
| 28 | 3.30 | 1.04 | 3.18 |
| 56 | 3.25 | 1.06 | 3.06 |



Shrinkage



Abrasion



<https://www.fhwa.dot.gov/publications/research/infrastructure/structures/06103/chapt3c.cfm>

| Specimen # | Mass Loss | |
|------------|--------------|--------------|
| | 22 Pound (g) | 44 Pound (g) |
| 1 | 11.3 | 23.4 |
| 2 | 10.9 | 31.5 |

- Measured wear depth less than 1 mm
- Wear depth less than 2 mm - Grade 2 high performance structural concrete

Absorption

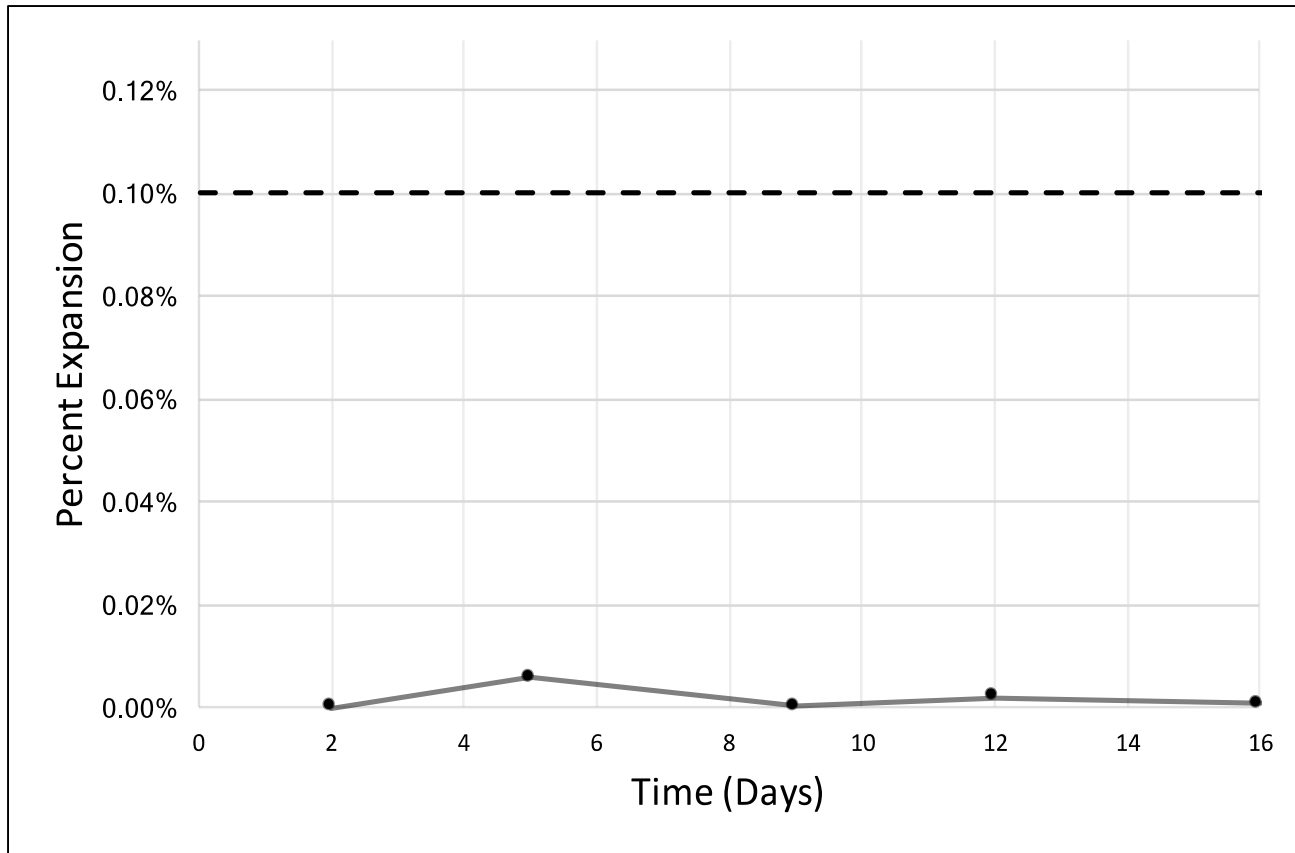


http://www.ctre.iastate.edu/pubs/en_route/07summer/cptech-lab.htm

| Specimen | Void Volume |
|----------|-------------|
| 1 | 1.36% |
| 2 | 1.30% |

- void volume < 12% will typically result in a durable concrete

Alkali Silica Reactivity



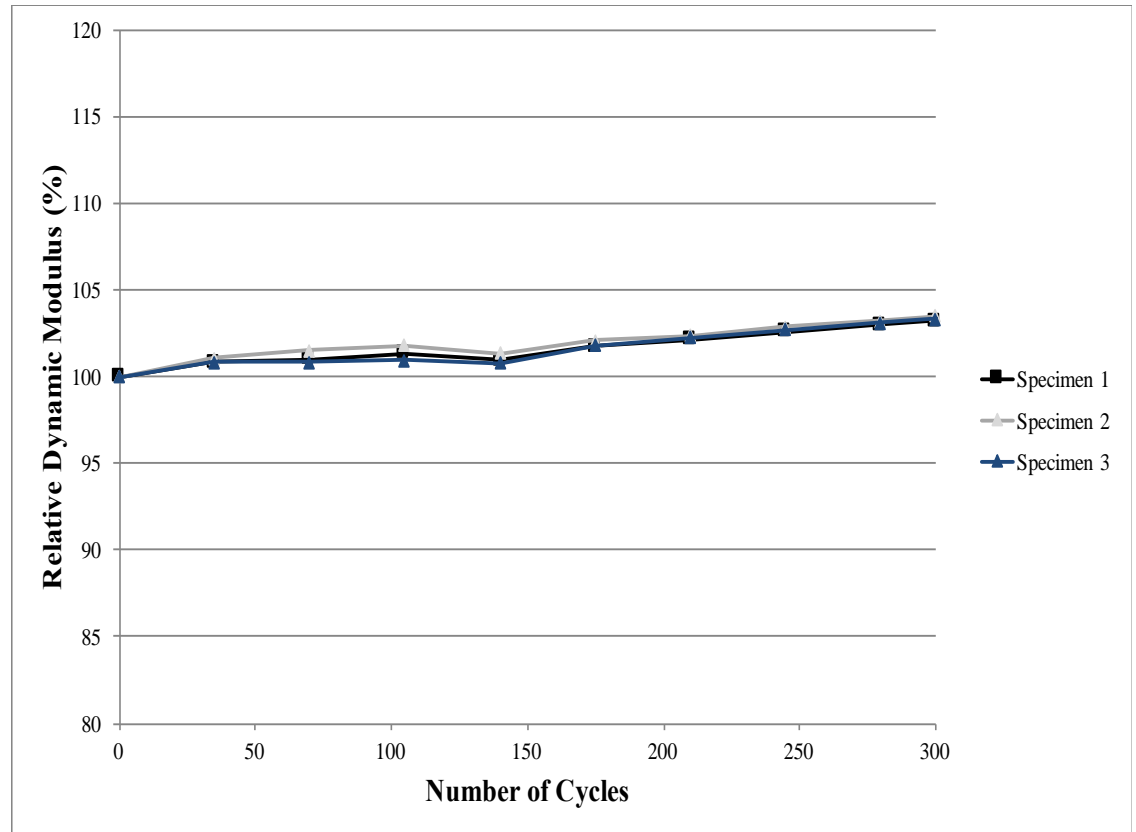
Chloride Permeability

| Mix | Age at Test (days) | Avg. Adj. Charge Passed (coulombs) | Chloride Ion Penetrability |
|------------|--------------------|------------------------------------|----------------------------|
| Specimen 1 | 56 | 75 | Negligible |
| Specimen 2 | 56 | 56 | Negligible |

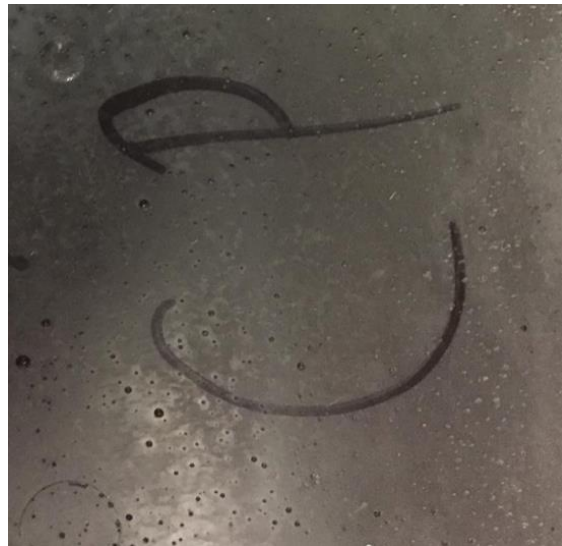
- Low Chloride Perm Range:
1000-2000 coulombs

Freeze-Thaw Resistance

| Specimen # | # of Cycles | Mass Change (%) | Durability Factor |
|------------|-------------|-----------------|-------------------|
| 1 | 300 | -0.089 | 103.2 |
| 2 | 300 | -0.096 | 103.5 |
| 3 | 300 | -0.066 | 103.4 |



Scaling



0 Cycles



50 Cycles

Conclusions

- Suitable materials for UHPC readily available in Montana
 - Type I/II portland cement from CRH in Trident, MT
 - fine masonry sand from Billings Quikrete
 - class F fly ash from the Coal Creek Station, ND
 - silica fume sourced through BASF
 - a high range water reducer (HRWR) sourced from CHRYSO
 - steel fibers from Nycon
- Response Surface Methodology Efficient/Effective Tool
 - characterizing the effect of the various constituents
 - optimization

Conclusions

- UHPC Sensitive to Various Parameters
 - batch size and mixer type
 - need fixed-drum rotating-fin mixer
 - specimen preparation technique
 - continuously agitate and cover to prevent moisture loss
 - cut ends off prior to grinding – over cast and grind top off in field
- Excellent Mechanical and Durability Properties
- Non-proprietary Economical UHPC Feasible in Montana

Recommendations

- Future Research to Investigate
 - Scaled-up mixes
 - batch sizes and equipment that would be used in the field (e.g., high-shear pan mixer)
 - various mixing conditions (e.g., temperatures and aggregate moisture conditions)
 - sensitivity to material variations
 - Confirm performance in proposed application
 - reduced development lengths
 - static and cyclic pull-out tests
 - Field demonstration project
 - potentially at Transcend in Lewistown

Thank you!